SOLID OXIDE MEMBRANE PROCESS FOR THE REDUCTION OF OXIDES IN SPENT NUCLEAR FUEL

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2012 International Pyroprocessing Research Conference
The Abbey Resort, Fontana, WI
August 26-30, 2012



Outline

- Overview of the SOM Process
 - SOM Process for Magnesium Production
 - SOM Process with Electrolytic Refining for Recycling Magnesium Alloys
 - SOM Process for Silicon Production
- SOM process for Uranium oxide reduction in spent nuclear fuel
 - Identify surrogate for Uranium oxide
 - Identify fluoride flux for dissolving the surrogate oxide
 - Determine stability of YSZ membrane in the chosen flux
 - Determine stability of reduced metal and flux-surrogate oxide system with cathode and crucible material
 - Perform and Characterize SOM electrolysis employing the flux with the surrogate oxide
 - Characterize Deposit and YSZ membrane
- Conclusions and Future Work

Schematic of the SOM Process for the Production of Metals

$$CH_4(g) + O^{2-}_{(YSZ)} \rightarrow CO(g) + 2H_2(g) + 2e^-$$

$$H_2(g) + O^{2-}_{(YSZ)} \rightarrow H_2O(g) + 2e^- \qquad C + O^{2-} \rightarrow CO(g) + 2e$$

$$CO(g) + O^{2-}_{YSZ} \rightarrow CO_2(g) + 2e^- \qquad O^{2-} \rightarrow \frac{1}{2} O_2(g) + 2e$$

$$Anode$$

$$Anode$$

$$O^{2-}_{(melt)} \rightarrow O^{2-}_{(YSZ)}$$

$$Ionic Melt (Molten salt) with$$

$$Dissolved MeO/Me'O$$

$$Me^{2+}_{(melt)} + 2e^- \rightarrow Me$$

$$Me'^{2+}_{(melt)} + 2e^- \rightarrow Me$$

$$Me'^{2+}_{(melt)} + 2e^- \rightarrow Me'$$

$$Me' + MeO = Me'O + Me$$

$$Cathode$$

$$O^{2-}_{(Melt)} \rightarrow O^{2-}_{(YSZ)}$$

$$O^{2-}_{$$

SOM Process (Mg, Si, Yb, Ca, Ta, and Ti)

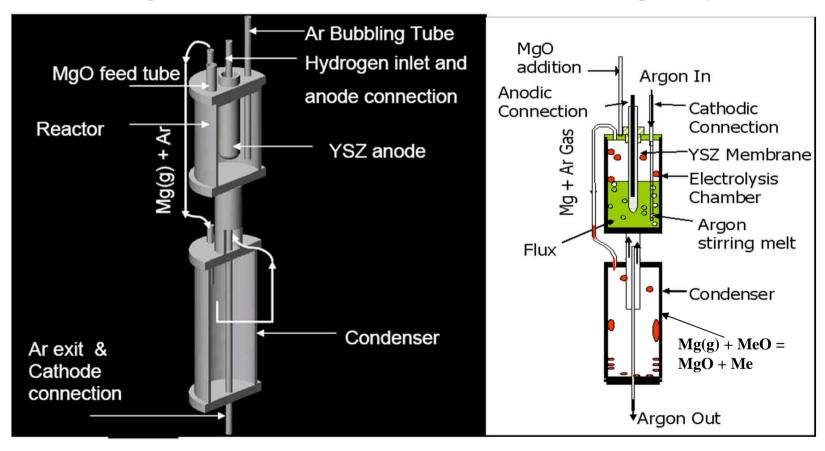
State-of-the-art Electrolysis

- Halide feed preparation
- Higher dissociation potential
- Higher energy requirement
- Environmentally Hazardous
 - Chlorine and its byproducts form at the anode
- Higher capital Cost

SOM Electrolysis

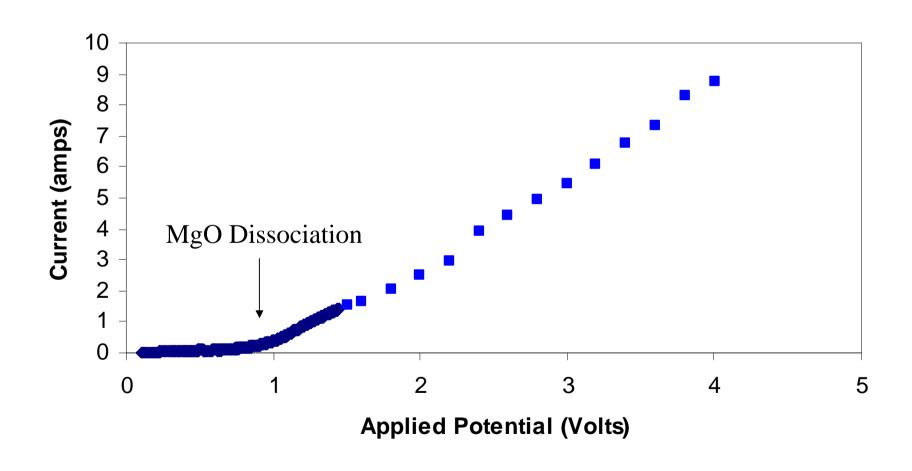
- Little or no oxide feed preparation
- Lower dissociation potential
- Lower energy requirement
- Environmentally friendly
 - Oxygen evolution at the anode
- Lower capital cost

Experimental Single Tube SOM Reactor for Magnesium Production(100-200 g/day)



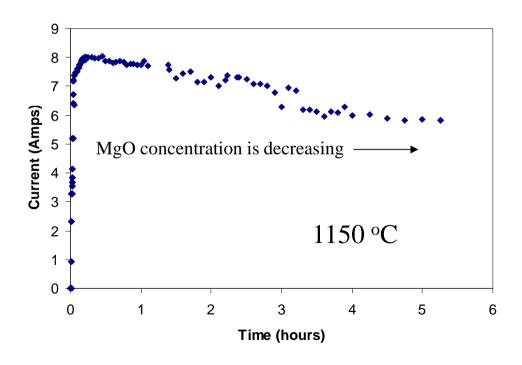
Stainless Steel construction; Single Tubular YSZ membrane; Separate chamber for Electrolysis and Condenser; 15 g/hr of Mg at 1 Amp/cm²; 1150 °C; 10 w% MgO in 55.5 w% MgF₂- CaF₂; Ar used as carrier and diluent for Mg vapor

Potentiodynamic Scan-Single Tube Reactor

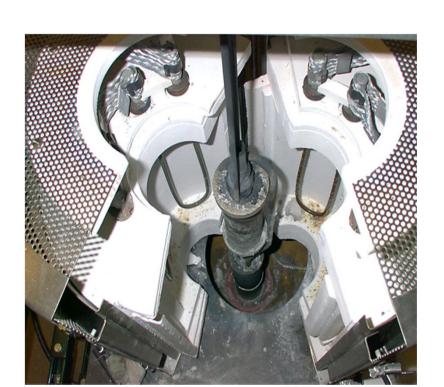


SOM Electrolysis of MgO-Single Tube Reactor

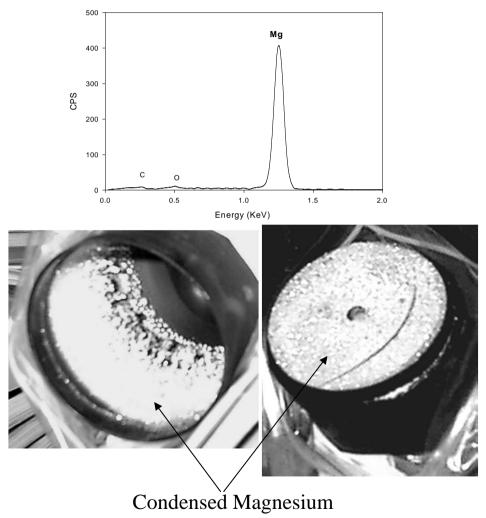
Potentiostatic Hold at 4.0 Volts



SOM Electrolysis of MgO

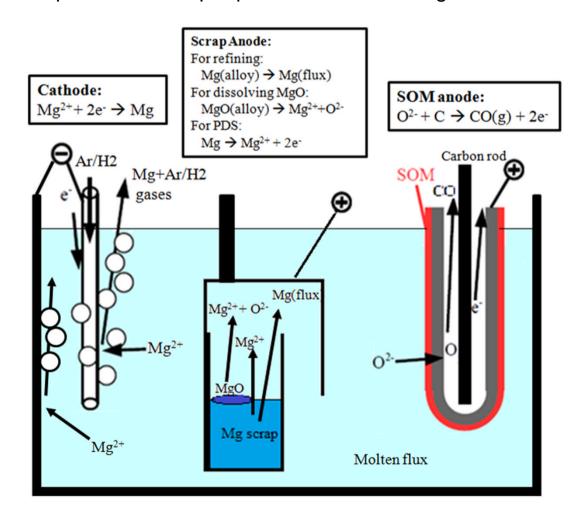


20 KV scan(2-4 micron penetration)



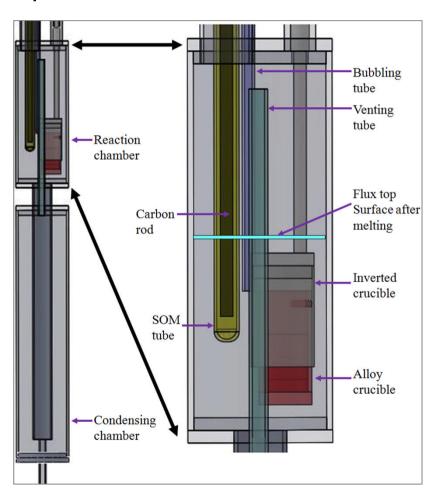
Combined SOM Electrolysis and Electrolytic Refining Processes for Recovering Magnesium from Partially Oxidized Magnesium Alloy Scrap

 Dissolve magnesium and its oxide from scrap into the flux, followed by cathodic deposition and vapor phase removal of magnesium



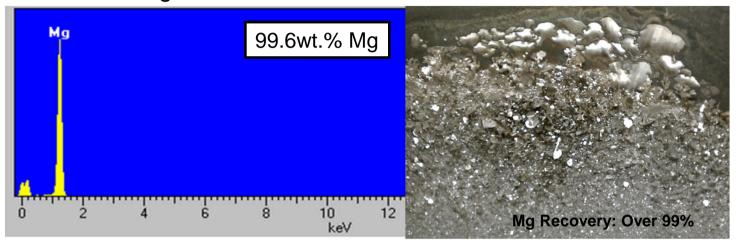
Magnesium Recovery from Partially Oxidized AZ91 Magnesium Alloy (90 w% Mg, 9 w% Al, 1 w% Zn): Combined SOM Electrolysis and Electrolytic Refining Process

Schematic of the setup:

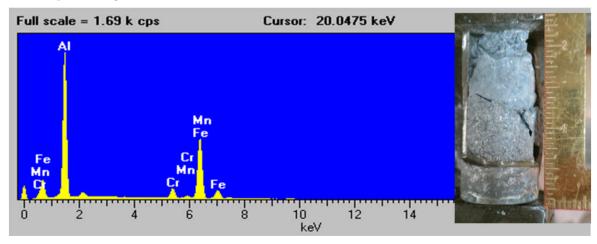


Energy-dispersive X-ray spectroscopy (EDS): Recovered Magnesium from the Scrap AZ91 Alloy

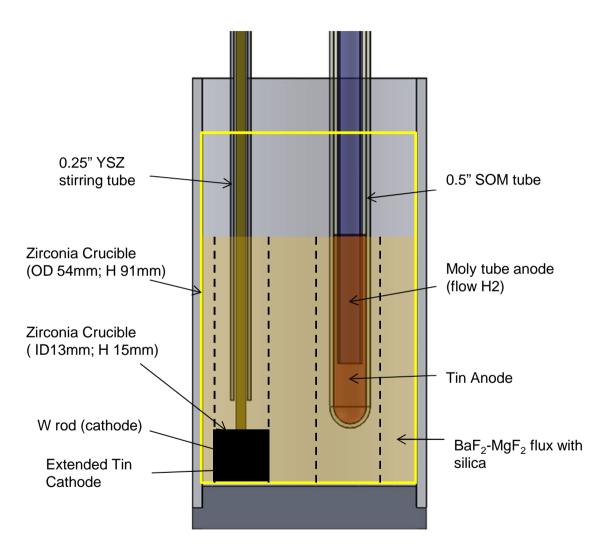
Recovered magnesium in the condenser



Scrap alloy residue

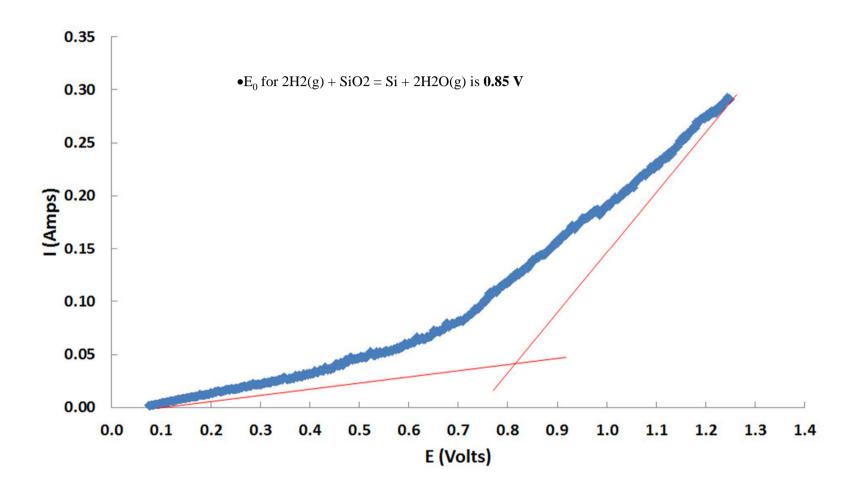


Schematic of Setup for Si-SOM Experiments

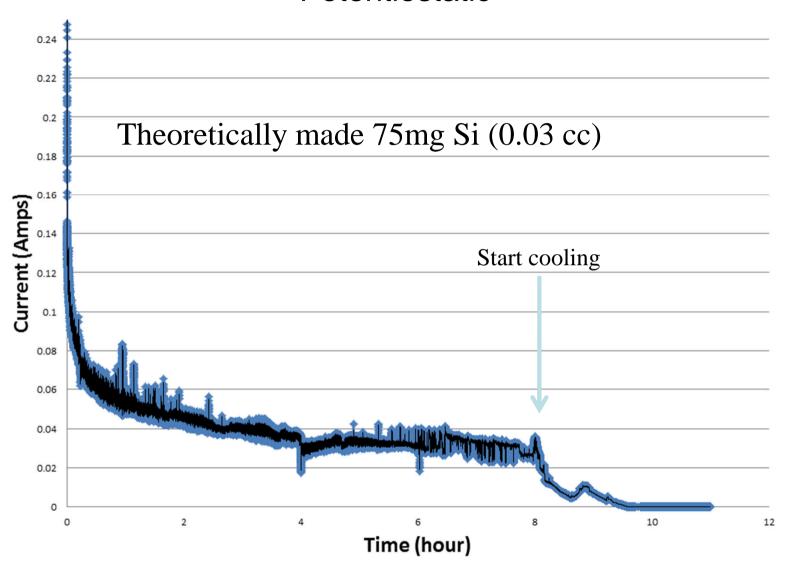


- Operating temperature 1070 C
- Si deposit was found on the surface of Tin cathode

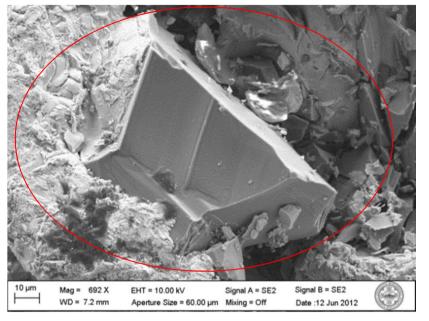
Current-voltage relationship for Silica Dissociation

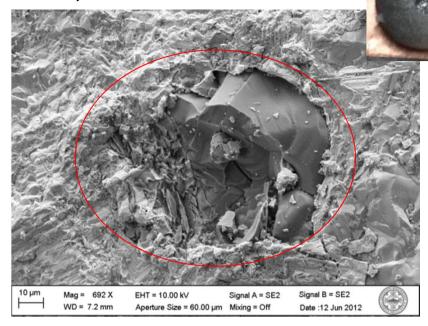


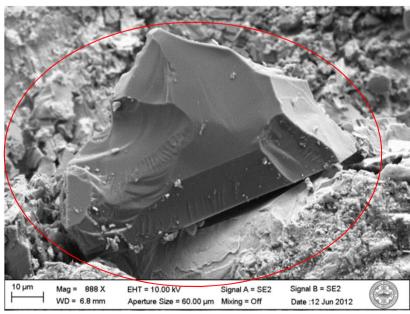
Potentiostatic

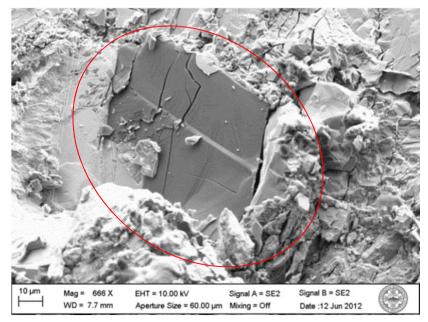


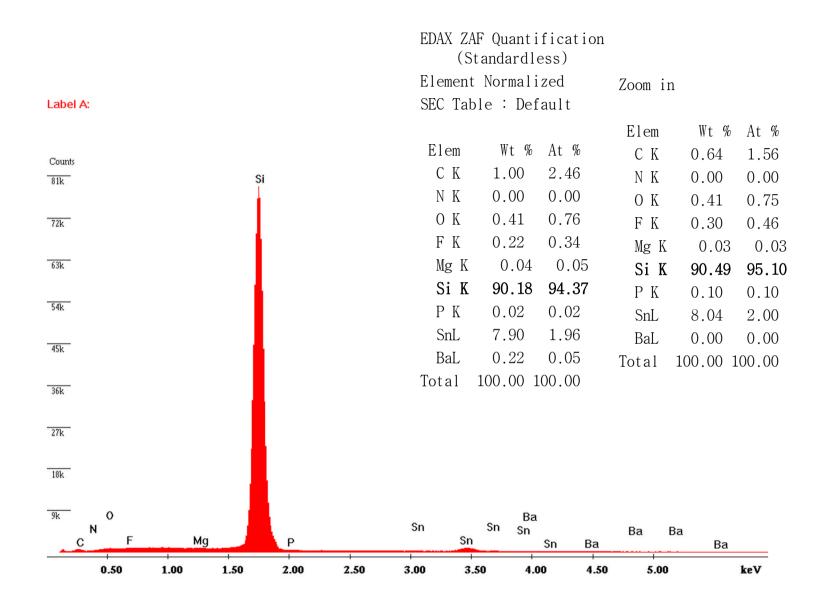
SEM image of Si deposits (Sn surface)



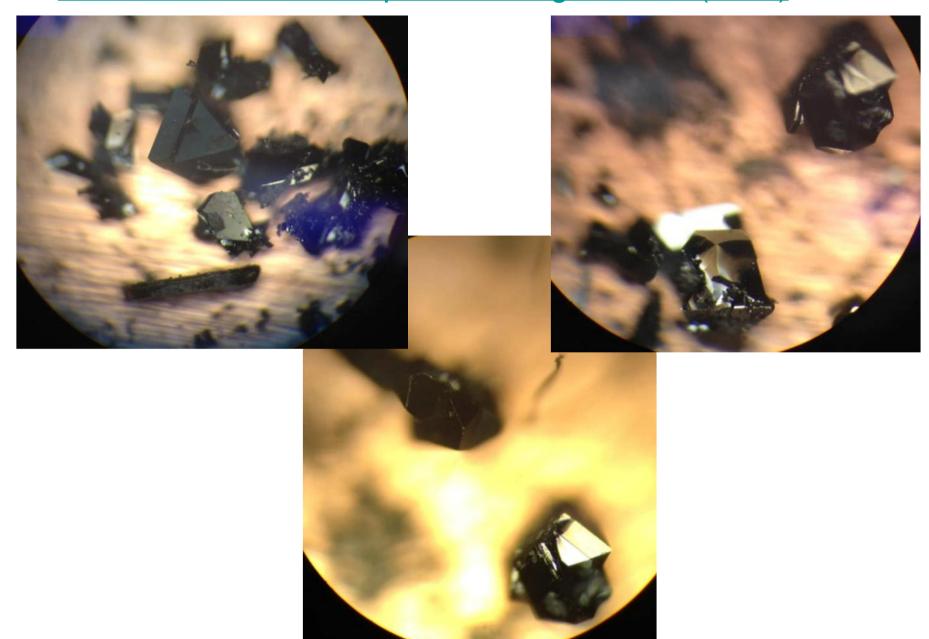








Extracted Si After Complete Etching from Sn (100x)



Selection of Ytterbium as a Surrogate for Uranium

At.	Element (M)	Valence	Atomic Radius (pm)	Electrons Per shell	Melting /Boiling point of fluorides (C)				
No					MF2	MF3	MF4	MF5	MF6
92	Uranium (mp-1132 C) (bp-4129 C)	2,3,4,5,6	156	2,8,18,32,21,9,2 (f block)		1427 and 1977	1036 and 1417	327 and 727	64.05 (TP)
70	Ytterbium (mp-824 C) (bp-1193 C)	2, <u>3</u>	176	2,8,18,32,8,2 (f block)	1052 and 2380	1157 and 2263			
58	Cerium (mp-798 C) (bp-3443 C)	<u>3</u> ,4	181	2,8,18,19,9,2 (f block)		1430 and 2327	977 and 1727		
63	Europium (mp-826 C) (bp-1529 C)	<u>2</u> ,3	180	2, 8, 18, 25, 8, 2 (f block)	1298 and 2427	1276 and 2277			
73	Tantalum (mp-3014 C) (bp-5453 C)	3,4,5	147	2,8,18,32,11,2 (d block)	1237 and 1977	1477 and 2077		95 and 229	
22	Titanium (mp-1668 C) (bp-3287 C)	2,3,4	147	2,8,10,2 (d block)	1277 and 2152	1200 and 1400	377		

Fluoride Flux Preparation

Thermogravimetry DTA Measurements

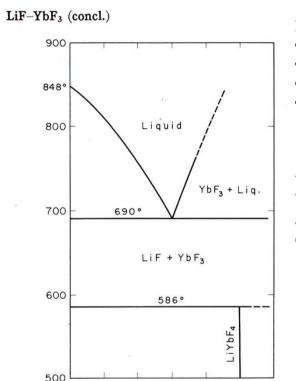


FIG. 3379.—System LiF-LiYbF₄.

G. A. Bukhalova and E. P. Babaeva, Zh. Neorgan. Khim., 11
[3] 624 (1966); Russ. J. Inorg. Chem. (English Transl.), 339

Mol. %

20

LiF

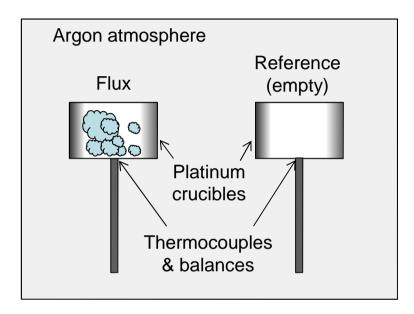
40

YbF3-

LiF-YbF₃-Yb₂O₃

- •0 w% Yb₂O₃
- •2 w% Yb₂O₃
- •5 w% Yb₂O₃3
- •10 w% Yb₂O₃

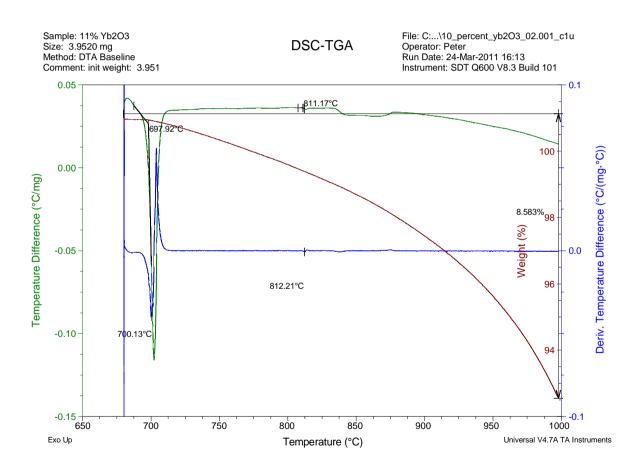
Mix, melt and quench 70 mole%LiF–30mole% YbF₃ with desired amounts of Yb₂O₃ in a controlled environment



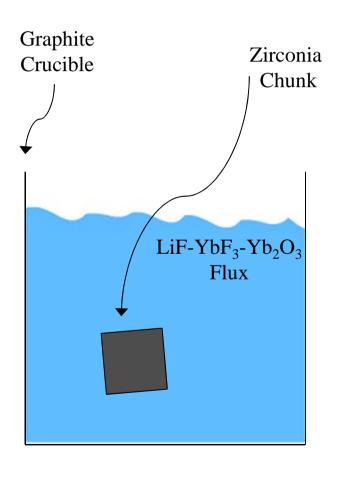
- •Heat flux and reference at a constant rate to 1000 C
- •Note difference in temperature and weight between flux and reference during heatup (determine liquidus)
- •Cool flux and reference at a constant rate to 500 C and note difference in temperature between flux and reference (reconfirm liquidus)

DTA-TFA Data

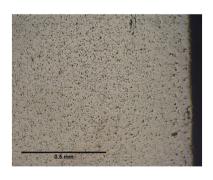
11 wt% Yb2O3 solubility in flux below 820 C (Yb melting point)



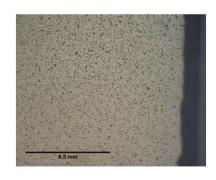
Determine Stability of YSZ Membrane in Flux



Place a chunk of YSZ membrane in the flux (LiF₂-YbF₃-Yb₂O₃) at 820 C for 5 hours



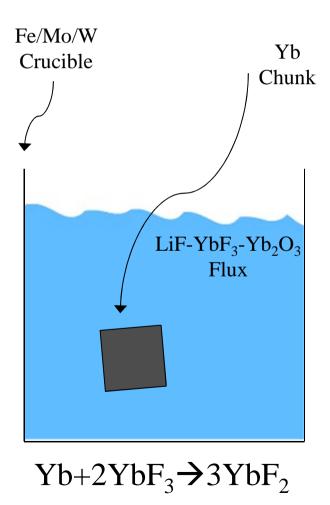
Section of YSZ in Flux

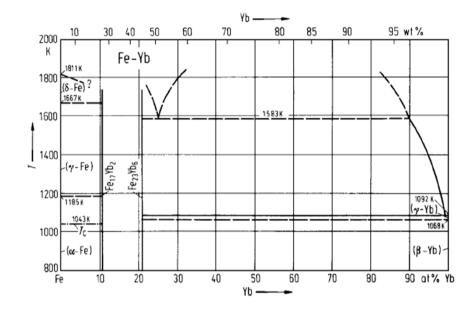


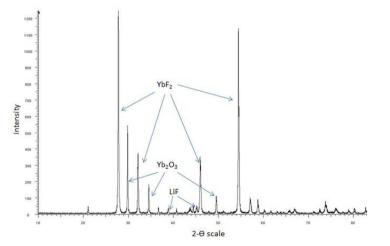
Section of Original YSZ

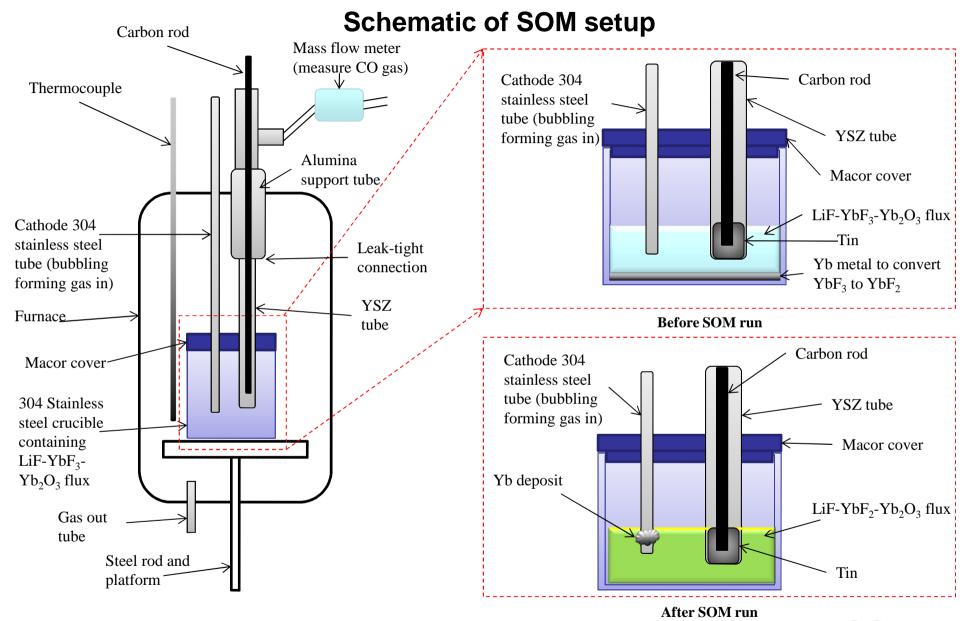
Determine Stability of Fe Crucible/Cathode with Flux and Yb

Place a chunk of Yb in the flux (LiF₂-YbF₃-Yb₂O₃) at 100 C above its liquidus in the Fe crucible for 5 hours



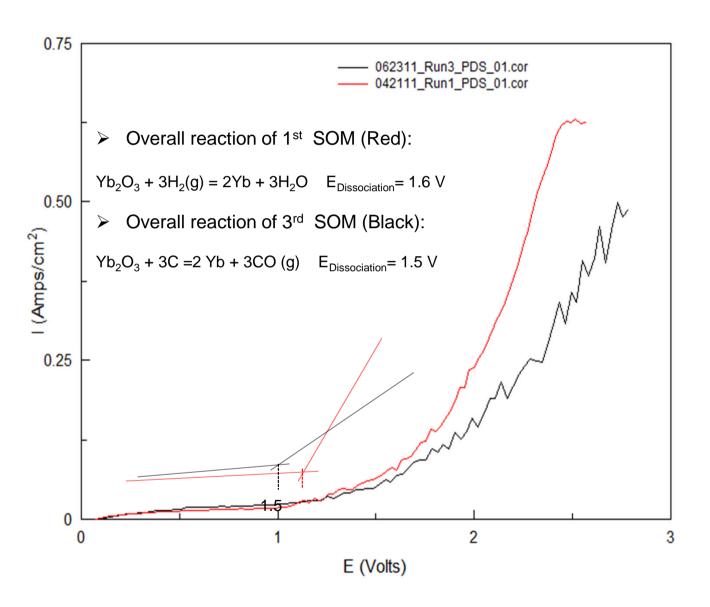






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Potentiodynamic scan (PDS)



Potentiostatic Measurement and CO Evolution 0.75 5 062311_Run3_PS_1228.cor 062311_Run3_PS_1640.cor 4.5 Rate of COgas formation (cc/min) 2nd PS 3.5 0.50 1** PS I (Amps/cm²) 3 2.5 CO from 2nd PS 1.5 CO from 1st PS 0.5 15000 5000 10000 Time (Sec)

Efficiency of Electrolysis

Weight loss of carbon rod: 0.27 g



$$Yb_2O_3 +3C = 2Yb + 3CO (g)$$

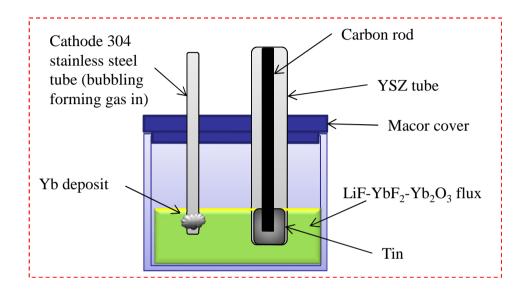
- Assuming 100% Faradic efficiency, theoretical amount of Yb produced based on measured current: 3.24 g
- Amount of Yb produced based on CO measurement: 2.04 g
- 3. Amount of Yb produced based on carbon rod weight loss: 2.60 g

Electrolysis efficiency

$$\frac{2.04}{3.24} = 63\%$$

$$\frac{2.60}{3.24} = 80\%$$

Metal Deposit on Cathode



Operating temperature for SOM: 800° C

Melting point of Yb : 819 $^{\circ}$ C

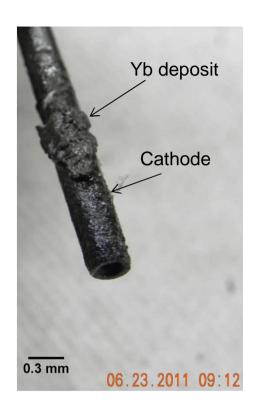
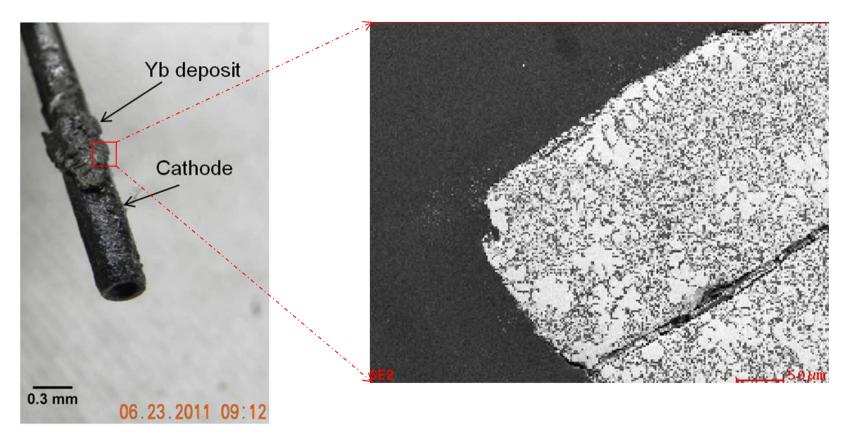


Photo of Yb deposit

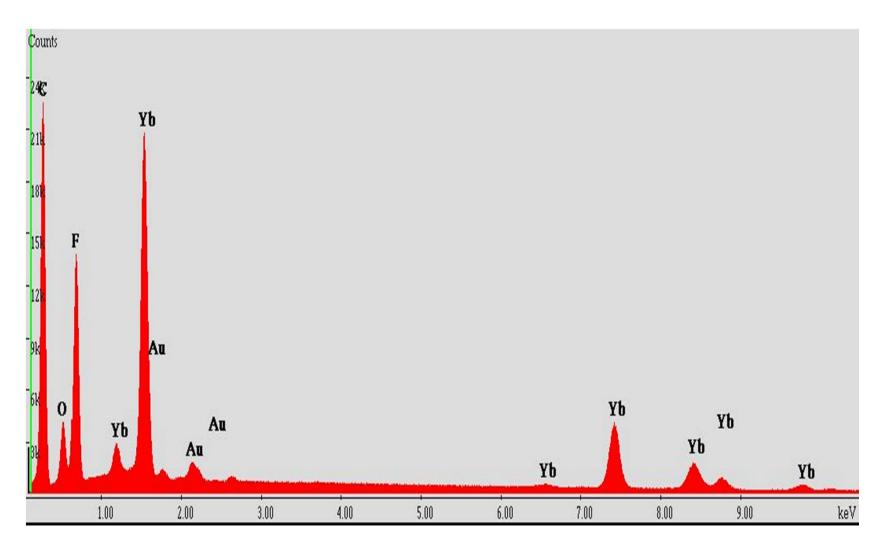
Metal Deposit on Cathode



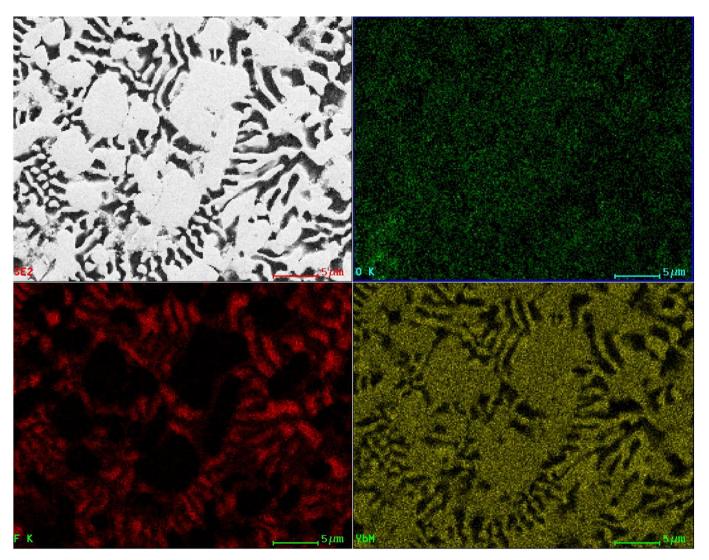
Metal deposit

SEM Image of the Deposit

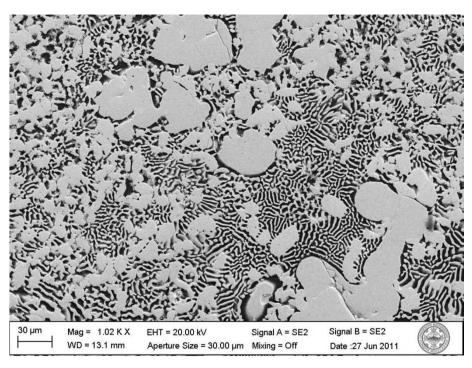
EDS Spectrum of the Metal Deposit

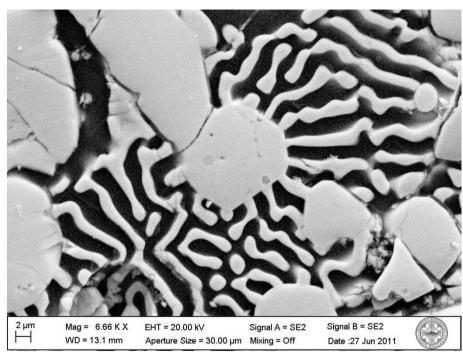


X-ray Maps confirm Yb metal deposit

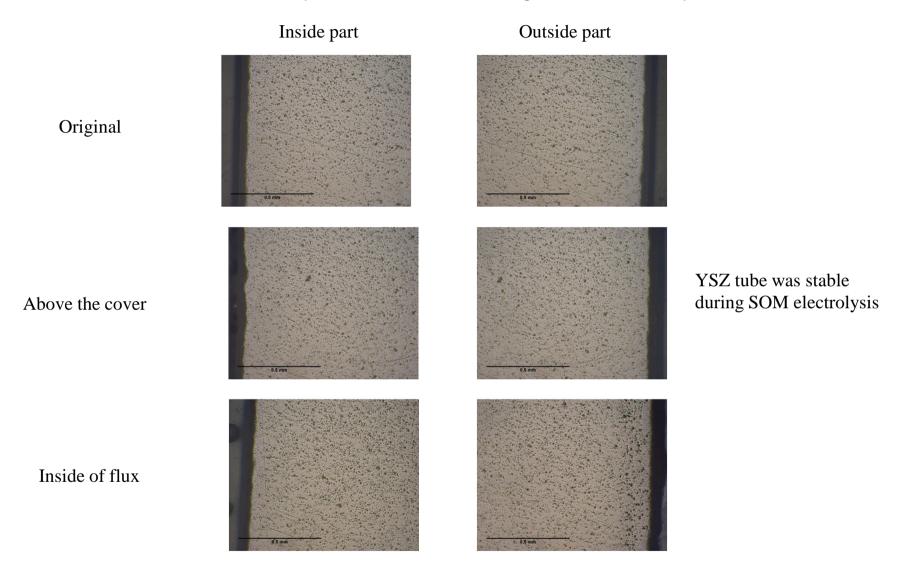


SEM Image of the Deposit Under Different Magnifications





Stability of YSZ Tube During SOM Electrolysis



Summary (SOM Process for Yb Production)

- Ytterbium oxide was reduced by the SOM Process
- Identified a low melting (700 C) and stable flux system (21 w% LiF and 79 w% YbF₃) for use in the SOM process. The flux dissolved 11 w% Yb₂O₃.
- Confirmed that the yttria-stabilized zirconia (YSZ) tube used as the solid oxide membrane was stable in the flux system for the duration of the experiment.
- Established a process for successfully lowering the valence state of Yb from 3+ to 2+ prior to producing the Yb metal by the SOM electrolytic process.
- Used carbon as the anodic feed and successfully measured the efficiency of the SOM electrolytic process.

Future Work (SOM Process)

- Investigate long-term stability of stabilized zirconia
- Quantify volatility of flux and the resultant change in flux composition
- Quantify process efficiency using real-time chemical analysis
- Explore impurity removal (more electronegative elements) prior to metal deposition
- Perform SOM electrolysis of more multivalent metals (transition metals)
- Investigate use of alternate anodes (oxygen producing inert anodes)
- Perform process modeling and scaleup.

ACKNOWLEDGEMENTS

My past and present students and post-doctoral fellows

David Woolley, Christopher Manning, Adam C. Powell, Ajay Krishnan, Timothy Keenan, Marko Suput, Rachel Delucas, Kyung Joong Yoon, Soobhankar Pati, Eric Gratz, Alex Roan, Xiaofei Guan, Yihong Jiang, Jiapeng Xu, Jarrod Milshtein, and Peter A. Zink

My past and present research sponsors

NSF, DOE, Safe Hydrogen, PNNL, INL, and MOxST